

(19)



Europäisches Patentamt

European Patent Office

Office européen des brevets



(11) Publication number:

**0 304 843 B1**

(12)

## EUROPEAN PATENT SPECIFICATION

- (45) Date of publication of patent specification: **03.03.93** (51) Int. Cl.<sup>5</sup>: **C08L 33/14**, C08L 27/16,  
/(C08L33/14,27:16),(C08L27/16,  
33:14)  
(21) Application number: **88113619.6**  
(22) Date of filing: **22.08.88**

The file contains technical information submitted  
after the application was filed and not included in  
this specification

### (54) Rubber composition.

(30) Priority: **24.08.87 JP 209697/87**

(43) Date of publication of application:  
**01.03.89 Bulletin 89/09**

(45) Publication of the grant of the patent:  
**03.03.93 Bulletin 93/09**

(84) Designated Contracting States:  
**DE FR**

(56) References cited:  
**EP-A- 0 194 030**

(73) Proprietor: **DENKI KAGAKU KOGYO  
KABUSHIKI KAISHA**  
4-1, Yuraku-cho 1-chome  
Chiyoda-ku Tokyo(JP)

(72) Inventor: **Kondo, Takeo** **Denki Kagaku Kogyo  
K.K.**  
**Kobunshi Kaihatsu Kenkyusho 3-5-1 Asahi-  
machi**  
**Machida-shi Tokyo(JP)**  
Inventor: **Miyagawa, Jiro** **Denki Kagaku Kogyo  
K.K.**  
**Kobunshi Kaihatsu Kenkyusho 3-5-1 Asahi-  
machi**  
**Machida-shi Tokyo(JP)**  
Inventor: **Shinohara, Katsuaki** **Denki Kagaku  
Kogyo K.K.**  
**Kobunshi Kaihatsu Kenkyusho 3-5-1 Asahi-  
machi**  
**Machida-shi Tokyo(JP)**

(74) Representative: **Wächtershäuser, Günter, Dr.**  
**Tal 29**  
**W-8000 München 2 (DE)**

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid (Art. 99(1) European patent convention).

**EP 0 304 843 B1**

## Description

The present invention relates to a rubber composition having excellent durability. More particularly, it relates to a rubber composition of a cured blend of an acrylic elastomer and a polyvinylidene fluoride resin.

Heretofore, for rubber parts to be in contact with fuel oil, rubber material has been selected for use so that the durability will not be impaired even when it is used in contact with such oil. For example, for fuel oil hoses, it has been common to use nitrile rubber (NBR) or hydrine rubber (CO and ECO) which has good oil resistance. However, as a result of the advent of an alcohol-added gasoline (hereinafter referred to as "gasohol") under the fuel situation in recent years, there has been a problem of a deterioration of rubber, particularly a problem of the volume change after immersion in gasohol. For this reason, NBR, CO and ECO are inadequate in the gasoline resistance against various gasolines, for use as fuel oil hoses. A material having improved durability has been desired.

EP-A-0 194 030 discloses a vulcanizable rubber composition comprising a vinylidene fluoride resin and an acrylic rubber containing a copolymerized crosslinkable monomer, which can be cured with a curing system comprising an organic peroxide.

The vulcanized rubber material shows durability against gasohol. However, the heat resistance of the material is not satisfactory.

It is an object of the present invention to provide a material having high durability, particularly improved durability against gasohol for e.g. fuel oil hoses for automobiles.

The present invention provides a rubber composition obtained by curing with a peroxide a blend comprising 100 parts by weight of an acrylic elastomer which does not contain a copolymerized crosslinkable monomer and from 20 to 100 parts by weight of a polyvinylidene fluoride resin. This composition has high durability particularly against gasohol and is useful for various applications under various severe conditions.

Now, the present invention will be described in further detail.

The acrylic elastomer to be used for the rubber composition of the present invention is preferably an elastomer obtained by polymerizing from 80 to 100% by weight of an alkoxyalkyl acrylate, from 0 to 20% by weight of acrylonitrile, from 0 to 5% by weight of ethylene and from 0 to 5% by weight of a vinyl fatty acid.

A preferred acrylic elastomer is the one obtained by polymerizing from 80 to 100% by weight of an alkoxyalkyl acrylate and from 0 to 20% by weight of acrylonitrile. A particularly preferred acrylic elastomer is the one obtained by polymerizing from 85 to 95% by weight of an alkoxyalkyl acrylate and from 5 to 15% by weight of acrylonitrile.

The respective components of the acrylic elastomer will be described.

The alkoxyalkyl acrylate may preferably be 2-methoxymethyl acrylate, 2-ethoxymethyl acrylate, 2-methoxyethyl acrylate, 2-ethoxyethyl acrylate and 2-butoxyethyl acrylate.

Acrylonitrile is effective for improvement of the fuel oil resistance of the rubber composition. However, if it exceeds 20% by weight, the cold resistance of the composition deteriorates.

Ethylene is effective for improvement of the cold resistance of the rubber composition. However, if it exceeds 5% by weight, the fuel oil resistance deteriorates.

The vinyl fatty acid is effective for improvement of the fuel oil resistance and heat resistance of the rubber composition. However, if it exceeds 5% by weight, the cold resistance and the alcohol-added fuel oil resistance deteriorate.

The polyvinylidene fluoride resin to be used in the present invention includes polyvinylidene fluoride and a copolymer of vinylidene fluoride with other copolymerizable monomer. Such other copolymerizable monomer includes hexafluoropropylene, pentafluoropropylene, trifluoroethylene, trifluorochloroethylene, tetrafluoroethylene, vinyl fluoride, perfluoro(methyl vinyl ether), perfluoro(propyl vinyl ether), other olefins and acrylic acid esters. One or more such copolymerizable monomers may be employed for the copolymerization.

The blend ratio of the acrylic elastomer and the polyvinylidene fluoride resin is 100 parts by weight of the former and from 20 to 100 parts by weight of the latter. If the polyvinylidene fluoride resin is less than 20 parts by weight, the improvement in the alcohol-added fuel oil resistance of the rubber composition will be inadequate, and if it exceeds 100 parts by weight, the cold resistance tends to be lost.

It is essential to use a peroxide for the curing of the blend, since no good cured product will be obtained with other curing agent commonly employed for the curing of usual acrylic elastomers.

For the preparation of an acrylic elastomer, it is common to employ a method wherein a monomer curable by a certain specific curing agent is copolymerized and the curing is conducted by means of such a specific curing agent. However, such a method is not suitable for the purpose of the present invention,

since the heat resistance of the cured product will thereby be inadequate. It is a feature of the acrylic elastomer of the present invention that no such a curable monomer is copolymerized. The blend of the present invention can readily be cured (or cross-linked) with a peroxide, and the cured (or cross-linked) rubber composition has good heat resistance.

5 As the peroxide, it is possible to employ any peroxide which is commonly useful for the curing of rubber. It includes, for example, di-t-butyl peroxide, t-butylcumyl peroxide, dicumyl peroxide,  $\alpha,\alpha$ -bis(t-butylperoxyisopropyl)benzene, 2,5-dimethyl-2,5-di(t-butylperoxy)hexane, 2,5-dimethyl-2,5-di(t-butylperoxy)-hexyne-3, 1,1-bis(t-butylperoxy)-3,3,5-trimethylcyclohexane, n-butyl-4,4-bis(t-butylperoxy)valerate, 2,2-bis(t-butylperoxy)butane and 2,2-bis(t-butylperoxy)octane. However, the peroxide is not restricted to such  
10 specific examples.

The amount of the peroxide is not particularly limited, but it is usually within a range of from 1 to 10 parts by weight relative to 100 parts by weight of the acrylic elastomer.

When the blend of an acrylic elastomer and a polyvinylidene fluoride resin is cured with the peroxide, it is effective to incorporate a polyfunctional monomer. The amount of such a polyfunctional monomer is  
15 preferably not more than 15 parts by weight relative to 100 parts by weight of the acrylic elastomer. An excessive polyfunctional monomer is undesirable, since the flexibility of the cured product tends to be thereby lost. As the polyfunctional monomer, trimethylolpropane trimethacrylate or trimethylolpropane triacrylate is most effective, and triallyl isocyanurate, triallyl cyanurate, triallyl trimellitate, 1,6-hexanediol acrylate, triethylene glycol diacrylate, polyethylene glycol diacrylate, diallyl phthalate and 1,2-polybutadiene  
20 may also be used.

For the curing with the peroxide, it is effective to combine a radical scavenger or a thiourea derivative for balancing the physical properties of the cured product. The radical scavenger is used preferably in an amount of not more than 3 parts by weight relative to 100 parts by weight of the acrylic elastomer, and the thiourea derivative is used preferably in an amount of not more than 5 parts by weight.

25 If the radical scavenger is used excessively, the peroxide will be consumed, such being against the intended purpose of balancing the physical properties of the cured product. Likewise, if the thiourea derivative is used excessively, the physical properties of the cross-linked product tend to deteriorate. Therefore, it is advisable to use them alone or in combination within the above-mentioned ranges.

The radical scavenger may be a compound commonly employed as a polymerization inhibitor or an  
30 antioxidant, or sulfur or a sulfur-containing compound. Typical examples include phenothiazine, 2,6-di-t-butyl-p-cresol, sulfur and a sulfur compound such as a curing accelerator for rubber.

To the composition of the present invention, various additives such as a filler, a plasticizer, a processing aid and a stabilizer, which are commonly employed in the rubber industry, may be added depending upon the particular purpose of the composition.

35 The filler may be added preferably in an amount of from 5 to 300 parts by weight relative to 100 parts by weight of the acrylic elastomer to improve the blend condition and the processability, whereby effective blending can be conducted. Such a filler includes, for example, carbon black, silica, calcium carbonate, clay and talc.

As the plasticizer, the one which does not impair the object of the present invention, i.e. the one having  
40 affinity to the composition, such as an oligomer of an  $\alpha$ -olefin or polybutene, polyether or polyester, may be mentioned. The plasticizer is used usually in an amount of not more than 100 parts by weight relative to 100 parts by weight of the acrylic elastomer.

Further, to the composition of the present invention, other rubbers such as various rubbers having excellent fuel oil resistance, may be incorporated as the case requires.

45 For the preparation of the composition of the present invention, the above-mentioned materials may be kneaded at a temperature of at least the melting point of the polyvinylidene fluoride resin by a means commonly employed in the rubber industry, such as an open roll mill or an internal mixer.

According to the present invention, however, the polyvinylidene fluoride resin can be kneaded with the acrylic elastomer, optionally together with a filler, a plasticizer or other additives and a curing agent, at a  
50 temperature lower than the melting point of the polyvinylidene fluoride resin to obtain a compound stock. This method has a merit in that the secondary processing temperature of the compound stock thereby obtained to e.g. a hose is lower than the compound stock obtainable by a usual method i.e. blending at a temperature higher than the melting point of the polyvinylidene fluoride resin.

The curing method may be any method commonly employed in the rubber industry. The curing  
55 conditions vary depending upon the type of the peroxide to be used. However, the curing can usually be accomplished by maintaining the compound stock at a temperature of from 120 to 200 °C for from 2 to 200 minutes. The curing temperature is preferably at least the melting point of the polyvinylidene fluoride resin to obtain a uniform rubber composition.

It is preferred to conduct post curing by subjecting the cured product again to heat treatment in an air oven to obtain a stabilized cured product.

The rubber composition of the present invention is excellent particularly in the gasohol resistance and also has cold resistance and heat resistance, and thus it is extremely durable as a fuel oil resistant material.

This composition is suitable as a material for various hoses to be in contact with fuel oils such as fuel oil hoses, air hoses or various hoses for control, and for various fuel oil parts such as diaphragms, packings and gaskets.

Now, the usefulness of the present invention will be described in further detail with reference to Examples. However, it should be understood that the present invention is by no means restricted by these specific Examples.

A blend was prepared by a 20.32 cm (8 inch) roll and then sheeted, and the sheet was subjected to press-curing at 170°C for 20 minutes.

The physical properties of the cured product were measured in accordance with JIS K6301. Acrylate elastomers A and B used here were prepared as follows.

#### Acrylic elastomer A:

Into an autoclave, 43 kg of water, 4 kg of acrylonitrile, 36 kg of methoxyethyl acrylate, 700 g of each of Denka Poval B-05 and B-17 as polyvinyl alcohols, 60 g of sodium acetate, 2 g of ferrous sulfate, 4 g of ethylenediamine tetraacetate and 90 g of a co-catalyst were charged and mixed under stirring. The internal temperature of the autoclave was adjusted to 45°C, and the air at the above portion in the autoclave was substituted by nitrogen. From a separate inlet, an aqueous solution of a polymerization initiator was injected to initiate the polymerization, and the injection was completed in twelve hours. To the emulsion of the formed polymer, an aqueous sodium sulfate solution was added to solidify the polymer. The solidified polymer was washed with water, dehydrated and dried, and then tested as acrylic elastomer A.

#### Acrylic elastomer B:

Acrylic elastomer B was prepared in the same manner as the preparation of acrylic elastomer A except further adding 160 g of glycidyl methacrylate and 480 g of allyl glycidyl ether to the recipe of Acrylic elastomer A.

#### EXAMPLES 1 to 4 and COMPARATIVE EXAMPLES 1 to 6

300 g of acrylic elastomer A or B, and the blend components as identified in Table 1 or 2 other than the polyvinylidene fluoride resin (KYNAR 741) and the cross-linking agent, were kneaded by a 20.32 cm (8 inch) mixing roll adjusted to a roll temperature of 40°C. Then, at a roll temperature of 160°C, the polyvinylidene fluoride resin was blended thereto.

After completion of the blending, the roll temperature was lowered to 40°C, and the cross-linking agent was kneaded thereto, and the mixture was formed into a sheet having a thickness of from 2.2 to 2.4 mm.

This sheet was subjected to press-curing (cross-linking) at 170°C for 20 minutes to obtain a cured product. In the case of the press-cured product of Comparative Example 2 or 3, the product was further exposed at 170°C for 4 hours in a Geer oven, followed by curing to further cure the product.

The tests for the physical properties under a normal condition and for the heat resistance at 150°C and 175°C were conducted in accordance with JIS K6301.

The fuel oil resistance was determined by the volume change ( $\Delta V$ ) after immersion in Fuel C (isooctane/toluene = 50/50 by volume %) and in a mixture of Fuel C/ethanol = 80/20 by volume %, at 40°C for 70 hours.

The cold resistance was determined in such a manner that a test piece (thickness: 2mm, length: 15 cm, width: 1.5 cm) was left to stand in a constant temperature room of -30°C for 5 hours and then bent at an angle of 180 degree whereupon the presence (X) or absence (O) of breakage was examined.

It is evident from Table 1 that the composition of the present invention has an excellent heat resistant retention of elongation as compared with the composition wherein no peroxide is employed, and it also has good cold resistance, gasoline resistance and heat resistance.




As shown by Examples 2 to 4 in Table 2, with a rubber composition of the present invention wherein a blend comprising an acrylic elastomer and a polyvinylidene fluoride resin is cured by a peroxide curing agent, the gasohol resistance is improved remarkably as the blend ratio of the polyvinylidene fluoride resin increases. However, if the proportion of the polyvinylidene fluoride resin in the blend exceeds 100 parts by

weight, the physical properties of the rubber tend to be poor and as such are not suitable for a rubber composition.

Table 1

	Example	Comparative Examples		
		1	2	3
Blend	100	100	—	—
	—	—	100	100
	25	25	25	25
	1	1	1	1
	1	1	1	1
	50	50	50	50
	25	25	25	25
	2	—	2	—
	0.5	—	0.5	—
	0.5	—	0.5	—
Blend	8	—	8	—
	4	4	—	—
	5)	—	—	—
	6)	—	—	—
	Phenothiazine	—	—	—
	V-40	—	—	—
	Accelerator DT	—	—	—
	A B	—	—	—
	8)	—	—	—
	2	—	—	—

Table 1 (Continued)

	Example	Comparative Examples			Comments
		1	2	3	
Physical properties under a normal condition	100% Modulus (kg/cm <sup>2</sup> )	30	44	33	press-curing 20 minutes at 170°C
	Tensile strength (kg/cm <sup>2</sup> )	76	93	102	
	Elongation (%)	290	210	320	
	Hardness (JIS- A)	63	65	62	
Fuel oil resistance	Fuel C $\Delta V$ (%)	9	9	9	70 hours at 40°C
	Fuel C/Ethanol (80/20) $\Delta V$ (%)	44	47	54	70 hours at 40°C
Cold resistance	-30°C Bending				
Heat resistance (175°C)	Retention (%) of strength	132	119	111	Gear oven 70 hours at 175°C
	Retention (%) of elongation	83	62	63	
	Change in hardness	+20	+20	+21	

Note: In Comparative Examples 2 and 3, after pressing at 170°C for 20 minutes, post curing was conducted in a Gear oven at 170°C for 4 hours.

Table 2

	Examples				Comparative Examples		
	2	3	4		4	5	6
KYNAR 741	25	50	100		0	10	150
Acrylic elastomer A	100	100	100		100	100	100
Stearic acid	1	1	1		1	1	1
Nauguard 445	1	1	1		1	1	1
Seast 116 9)	50	50	50		50	50	50
RS-700	25	25	25		25	25	25
Blend	2	2	2		2	2	2
	0.5	0.5	0.5		0.5	0.5	0.5
	0.5	0.5	0.5		0.5	0.5	0.5
	8	8	8		8	8	8
TMPT							
TMU							
Phenothiazine							
V-40							

Table 2 (Continued)

		Examples				Comparative Examples			Comments
		2	3	4		4	5	6	
Physical properties under a normal condition	100% Modulus (kg/cm <sup>2</sup> )	42	77	108		15	23		Press-curing 30 minutes at 170°C
	Tensile strength (kg/cm <sup>2</sup> )	85	111	127		81	80	133	
	Elongation (%)	250	230	220		430	370	110	
	Hardness (JIS- A)	62	81	86		39	52	94	
Cold deterioration resistance (50% destruction) (°C) -30°C Bending		-26	-26	-26		-28	-28	-17	
		○	○	○		○	○	×	
Fuel oil resistance	Fuel C ΔV (%)	10	7	1		20	15	0	70 hours at 40°C
	Fuel C/Ethanol ΔV (%) (80/20)	44	33	14		65	52	10	70 hours at 40°C
Heat resistance	Retention (%) of strength	105	103	105		104	104	111	Geer oven 70 hours at 150°C
	Retention (%) of elongation	84	80	86		81	82	73	
	Change in hardness	+ 5	+ 4	+ 7		+ 9	+ 8	- 4	

Note: The blend components used in the Examples and Comparative Examples were as follows:

- 1) Polyvinylidene fluoride, manufactured by Uniroyal Co.
- 2) Naugard 445, manufactured by Tokai Carbon Co.
- 3) HAF-LS carbon black, manufactured by Tokai Carbon Co.
- 4) Ester plasticizer, manufactured by Adeka Argus Co.
- 5) Trimethylolpropane trimethacrylate
- 6) Trimethylolpropane
- 7) Perhexa V-40, peroxide, manufactured by Nippon Yushi K.K., 40% 2,5-dimethyl-2,5-di(t-butylperoxy)hexane
- 8) Ammonium benzoate, manufactured by Ouchi Shinko Kagaku Kogyo K.K.
- 9) HAF carbon black, manufactured by Tokai carbon Co.



## EXAMPLE 5

## (1) Blending and compounding

5        1400 g of acrylic elastomer A (raw rubber) was changed into a 3 liter kneader and roughly kneaded for one minute. Then, the polyvinylidene fluoride resin (KYNAR 741, melting point: 165-170 °C, 50 mesh pass) and the rest of the blend components other than the curing agent were charged thereto, and the mixture was kneaded for 3 minutes. After sweeping up the ingredients around the hopper and adding them to the mixture, the mixture was kneaded again for 3 minutes, and the blend was discharged. The blend  
10 composition and the kneading temperature are shown in Table 3.

The discharged blend was sheeted at 40 °C by a 25.4 cm (10 inch) roll. After cooling, it was again wound on a 25.4 cm (10 inch) roll and kneaded with a curing agent (peroxide), and then formed into a sheet.

## 15 (2) Extrusion

By using an extruder with L/D = 400 mm/50 mm, a hose having an inner diameter of 9 mm and outer diameter of 13 mm was extruded at such a cylinder temperature as inlet/center portion/dye-mounting portion/dye head = 50/70/90/110 °C at a screw rotational speed of 20 rpm.

20

## (3) Curing

The curing was conducted under the curing conditions as shown in Table 3.

## 25 (4) Measurement of shrinkage of the extruded product

After curing by a steam autoclave under the press-curing (cross-linking) conditions as shown in Table 3, the shrinkage in the longitudinal direction of the hose (%) was measured.

## 30 (5) Physical properties

After the curing, the hose was left to stand at room temperature for one day, and then the respective physical properties were measured in accordance with JIS K6301. The results are shown in Table 3.

The solvent cracking growth and the fuel oil resistance were measured by the following methods.

35

(i) Solvent cracking growth:

A solvent mixture of isooctane and toluene with a volume ratio of 40:60 was maintained at 40 °C, and a dumbbell No. 1 according to JIS was punched out from the sample used for the measurement of the shrinkage of the extruded product, and a cut mark was made at the center of the dumbbell in the same manner as in the De Mattia bending test according to JIS K6301. Then, by adjusting the elongation at predetermined level, it was immersed in the solvent mixture, and the time until breakage was measured.

40

(ii) Fuel oil resistance:

45

The volume change ( $\Delta V$ ) after immersion in Fuel C (isooctane/toluene = 50/50 by volume %) and in a mixture of Fuel C/ethanol = 80/20 by volume %, at 40 °C for 70 hours, was measured.

50

55

Table 3

5			Example
			5
10	Blend	Acrylic elastomer A	100
		KYNAR 741 (Melting point: 165-170°C)	50
15		Stearic acid	1
		Nauguard 455	1
		Seast 6 10)	25
20		Asahi thermal 11)	35
		RS-107 12)	15
25		HV-100 13)	10
		TMPT	2
		TMU	0.5
30		Phenothiazine	0.5
		V-40	8

35

40

45

50

55

Table 3 (Continued)

5			Example
10			5
	Kneading	Kneader temperature (°C)	40
15	Curing condition	Temperature (°C)	170
		Time (min.)	30
20	Physical properties of cured product	100% Modulus (kg/cm <sup>2</sup> )	51
		Tensile strength (kg/cm <sup>2</sup> )	110
		Elongation (%)	390
25		Hardness (JIS-A)	77
30		Solvent cracking growth Elongation 50% (h) 40% (h)	0.2 > 24
35		Fuel oil resistance Fuel C resistance ΔV(%) Fuel C/EtOH resistance ΔV (%)	19 41
40		Shrinkage of the hose (%)	7

Note: Blend components other than mentioned above:

10) ISAF carbon black, manufactured by Tokai Carbon Co.

11) FT carbon black, manufactured by Asahi Carbon Co.

12) Ester plasticizer, manufactured by Adeka Argus Co.

13) Polybuten, manufactured by Nippon Sekiyu Kagaku K.K.

#### 50 Claims

1. A rubber composition obtained by curing with a peroxide, a blend comprising 100 parts by weight of an acrylic elastomer which does not contain a copolymerized cross-linkable monomer and from 20 to 100 parts by weight of a polyvinylidene fluoride resin.
2. The rubber composition according to Claim 1, wherein the acrylic elastomer comprises from 80 to 100 parts by weight of an alkoxyalkyl acrylate, from 0 to 20% by weight of acrylonitrile, from 0 to 5% by weight of ethylene and from 0 to 5% by weight of a vinyl fatty acid.

3. The rubber composition according to Claim 1, wherein the acrylic elastomer comprises from 80 to 100% by weight of an alkoxyalkyl acrylate and from 0 to 20% by weight of acrylonitrile.
4. The rubber composition according to Claim 3, wherein the acrylic elastomer comprises from 85 to 95% by weight of an alkoxyalkyl acrylate and from 5 to 15% by weight of acrylonitrile.
5. The rubber composition according to Claim 2, wherein the alkoxyalkyl acrylate is 2-methoxymethyl acrylate, 2-ethoxymethyl acrylate, 2-methoxyethyl acrylate, 2-ethoxyethyl acrylate or 2-butoxyethyl acrylate.
6. The rubber composition according to Claim 1, wherein the polyvinylidene fluoride resin is a homopolymer of vinylidene fluoride or a copolymer of vinylidene fluoride with other copolymerizable monomers selected from the group consisting of hexafluoropropylene, pentafluoropropylene, trifluoroethylene, trifluorochloroethylene, tetrafluoroethylene, vinyl fluoride, perfluoro(methyl vinyl ether), perfluoro(propyl vinyl ether), other olefins and acrylic acid esters.
7. The rubber composition according to Claim 1, wherein the blend is cured with from 1 to 10 parts by weight of the peroxide relative to 100 parts by weight of the acrylic elastomer.
8. The rubber composition according to Claim 1, wherein the blend comprises 100 parts by weight of the acrylic elastomer, from 20 to 100 parts by weight of the polyvinylidene fluoride resin, from 5 to 300 parts by weight of a filler and from 0 to 100 parts by weight of a plasticizer.
9. A process for producing a rubber composition of Claim 1, which comprises preparing a compound stock comprising the blend as defined in Claim 1 and the peroxide at a temperature lower than the melting point of the polyvinylidene fluoride resin and curing the blend with the peroxide at a temperature of at least the melting point of the polyvinylidene fluoride resin.
10. The rubber composition according to Claim 1, in the form of a hose, a diaphragm, a packing or a gasket to be in contact with a fuel oil.

#### Patentansprüche

1. Kautschukzusammensetzung, erhalten durch Härten einer Mischung, die 100 Gewichtsteile Acrylelastomer, das kein copolymerisiertes vernetzbares Monomer enthält, und 20 bis 100 Gewichtsteile Polyvinylidenfluorid-Harz umfaßt, mit einem Peroxid.
2. Kautschukzusammensetzung nach Anspruch 1, in der das Acrylelastomer 80 bis 100 Gewichtsteile Alkoxyalkylacrylat, 0 bis 20 Gew.-% Acrylnitril, 0 bis 5 Gew.-% Ethylen und 0 bis 5 Gew.-% Vinylfettsäure umfaßt.
3. Kautschukzusammensetzung nach Anspruch 1, in der das Acrylelastomer 80 bis 100 Gew.-% Alkoxyalkylacrylat und 0 bis 20 Gew.-% Acrylnitril umfaßt.
4. Kautschukzusammensetzung nach Anspruch 3, in der das Acrylelastomer 85 bis 95 Gew.-% Alkoxyalkylacrylat und 5 bis 15 Gew.-% Acrylnitril umfaßt.
5. Kautschukzusammensetzung nach Anspruch 2, in der das Alkoxyalkylacrylat 2-Methoxymethylacrylat, 2-Ethoxymethylacrylat, 2-Methoxyethylacrylat, 2-Ethoxyethylacrylat oder 2-Butoxyethylacrylat ist.
6. Kautschukzusammensetzung nach Anspruch 1, in der das Polyvinylidenfluorid-Harz ein Homopolymer von Vinylidenfluorid oder ein Copolymer von Vinylidenfluorid mit anderen copolymerisierbaren Monomeren, die aus der aus Hexafluorpropylen, Pentafluorpropylen, Trifluorethylen, Trifluorchlorethylen, Tetrafluorethylen, Vinylfluorid, Perfluor (methylvinylether), Perfluor(propylvinylether), anderen Olefinen und Acrylsäureestern bestehenden Gruppe ausgewählt sind, ist.
7. Kautschukzusammensetzung nach Anspruch 1, in der die Mischung mit 1 bis 10 Gewichtsteilen des Peroxids im Verhältnis zu 100 Gewichtsteilen des Acrylelastomers gehärtet ist.

8. Kautschukzusammensetzung nach Anspruch 1, in der die Mischung 100 Gewichtsteile des Acrylelastomers, 20 bis 100 Gewichtsteile des Polyvinylidenfluorid-Harzes, 5 bis 300 Gewichtsteile Füllstoff und 0 bis 100 Gewichtsteile Weichmacher umfaßt.
9. Verfahren zur Herstellung einer Kautschukzusammensetzung nach Anspruch 1, umfassend das Herstellen einer Vorratsmischung, die die wie in Anspruch 1 definierte Mischung und das Peroxid umfaßt, bei einer Temperatur, die niedriger als der Schmelzpunkt des Polyvinylidenfluorid-Harzes ist, und das Härten der Mischung mit dem Peroxid bei einer Temperatur von mindestens dem Schmelzpunkt des Polyvinylidenfluorid-Harzes.
10. Kautschukzusammensetzung nach Anspruch 1 in Form eines Schlauches, eines Diaphragmas, einer Dichtung oder einer Dichtscheibe, die in Kontakt mit einem Brennstofföl stehen sollen.

### Revendications

1. Composition de caoutchouc, obtenue par durcissement par un peroxyde, d'un mélange comprenant 100 parties en poids d'un élastomère acrylique qui ne contient pas de monomère réticulable copolymérisé, et 20 à 100 parties en poids d'une résine de poly(fluorure de vinylidène).
2. Composition de caoutchouc selon la revendication 1, dans laquelle l'élastomère acrylique comprend de 80 à 100 parties en poids d'un acrylate d'alcoxyalkyle, de 0 à 20% en poids d'acrylonitrile, de 0 à 5% en poids d'éthylène, et de 0 à 5% en poids d'un acide gras vinylique.
3. Composition de caoutchouc selon la revendication 1, dans laquelle l'élastomère acrylique comprend de 80 à 100% en poids d'un acrylate d'alcoxyalkyle et de 0 à 20% en poids d'acrylonitrile.
4. Composition de caoutchouc selon la revendication 3, dans laquelle l'élastomère acrylique comprend de 85 à 95% en poids d'un acrylate d'alcoxyalkyle et de 5 à 15% en poids d'acrylonitrile.
5. Composition de caoutchouc selon la revendication 2, dans laquelle l'acrylate d'alcoxyalkyle est le 2-méthoxyméthyl acrylate, le 2-éthoxyméthyl acrylate, le 2-méthoxyéthyl acrylate, le 2-éthoxyéthyl acrylate ou le 2-butoxyéthyl acrylate.
6. Composition de caoutchouc selon la revendication 1, dans laquelle la résine de poly(fluorure de vinylidène) est un homopolymère du fluorure de vinylidène ou un copolymère du fluorure de vinylidène avec d'autres monomères copolymérisables choisis dans le groupe constitué par l'hexafluoropropylène, le pentafluoropropylène, le trifluoroéthylène, le trifluorochloroéthylène, le tétrafluoroéthylène, le fluorure de vinyle, le perfluoro(méthyl vinyl éther), le perfluoro(propyl vinyl éther), d'autres oléfines et les esters de l'acide acrylique.
7. Composition de caoutchouc selon la revendication 1, dans laquelle le mélange est durci avec 1 à 10 parties en poids de peroxyde par rapport à 100 parties en poids de l'élastomère acrylique.
8. Composition de caoutchouc selon la revendication 1, dans laquelle le mélange comprend 100 parties en poids de l'élastomère acrylique, 20 à 100 parties en poids de la résine de poly(fluorure de vinylidène), 5 à 300 parties en poids d'une charge, et 0 à 100 parties en poids d'un plastifiant.
9. Procédé de fabrication d'une composition de caoutchouc telle que définie à la revendication 1, qui comprend la préparation d'une masse de mise en oeuvre comprenant le mélange tel que défini à la revendication 1 et le peroxyde à une température inférieure au point de fusion de la résine de poly(fluorure de vinylidène), et le durcissement du mélange à l'aide du peroxyde à une température d'au moins le point de fusion de la résine de poly(fluorure de vinylidène).
10. Composition de caoutchouc selon la revendication 1, sous la forme d'un tuyau souple, d'un diaphragme, d'une garniture ou d'un joint destiné à être en contact avec un fluide.

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ BLACK BORDERS
- ☐ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
- ☐ ~~FADED~~ TEXT OR DRAWING
- ☐ ~~BLURRED~~ OR ILLEGIBLE TEXT OR DRAWING
- ☐ SKEWED/SLANTED IMAGES
- ☐ COLOR OR BLACK AND WHITE PHOTOGRAPHS
- ☐ GRAY SCALE DOCUMENTS
- ☐ ~~LINE~~S OR MARKS ON ORIGINAL DOCUMENT
- ☐ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY
- ☐ OTHER: \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**